

# **Smart actuators/sensors based on magneto-elastic materials**

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# Lab.I.Ri.N.T.I. - University of Sannio



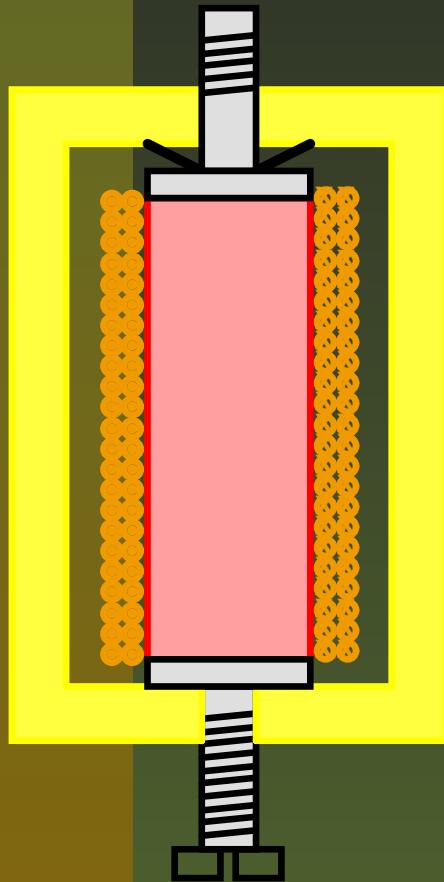
- magnetic characterization of samples
- mechanical characterization of materials (Young's Modulus, etc.)
- integrated characterization of electro-mechanical devices.
- main devices:
  - vectorial vibration sample magnetometer
  - compression-traction load test system (5kN)
  - integrated system for the generation of arbitrary magnetic field (computer controlled)

# Outline

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- Short introduction to magneto-elastic materials (Terfenol-D)
- A phenomenological approach to magneto-elastic devices design
- Example: a linear actuator
- Example: a linear magnetic field sensor
- Conclusions and foreseen

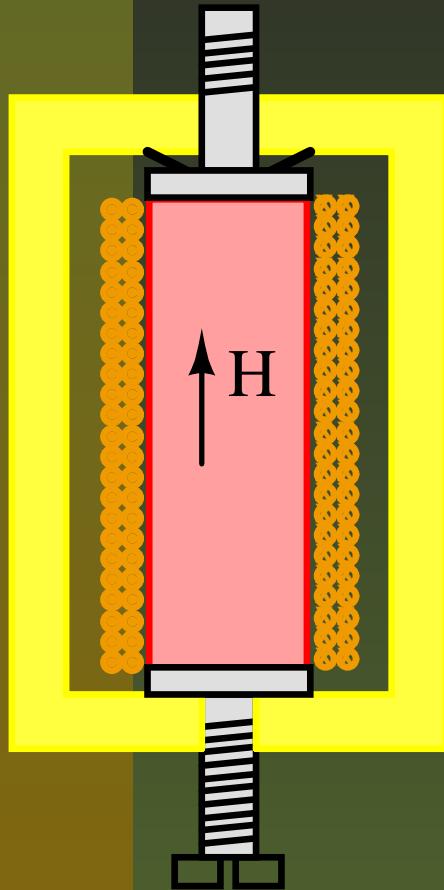
# Typical actuators with Terfenol-D



[www.energeninc.com](http://www.energeninc.com)



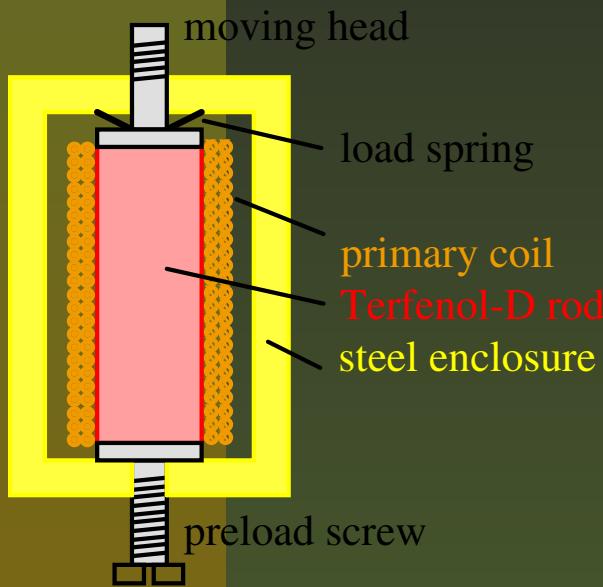
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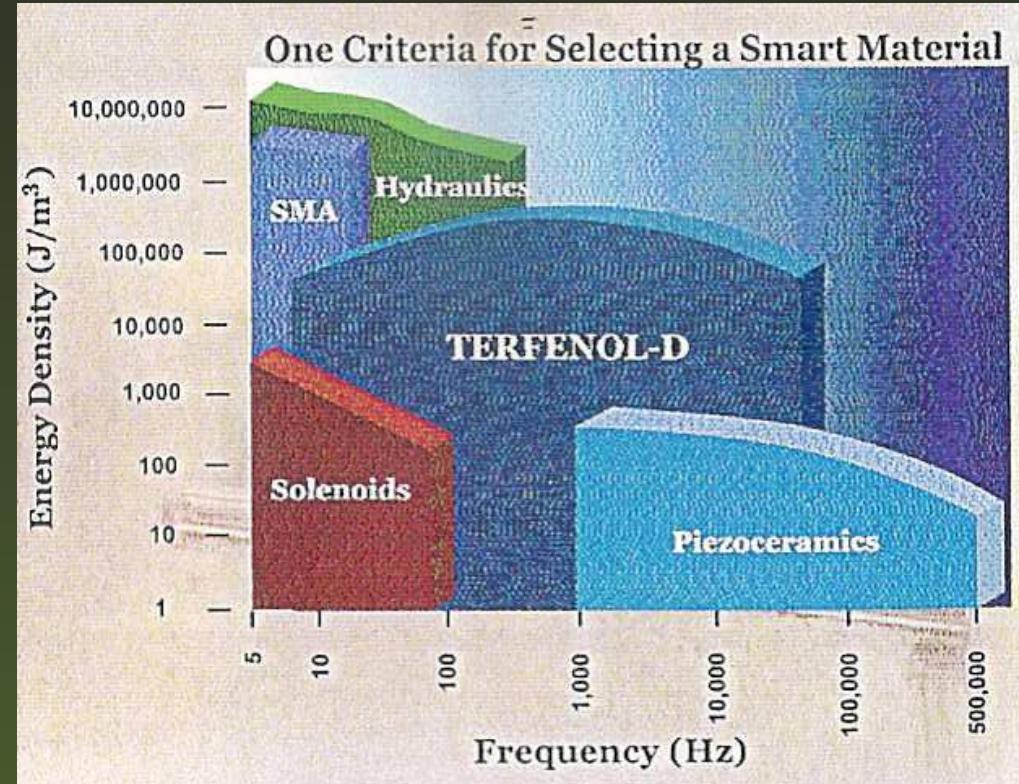
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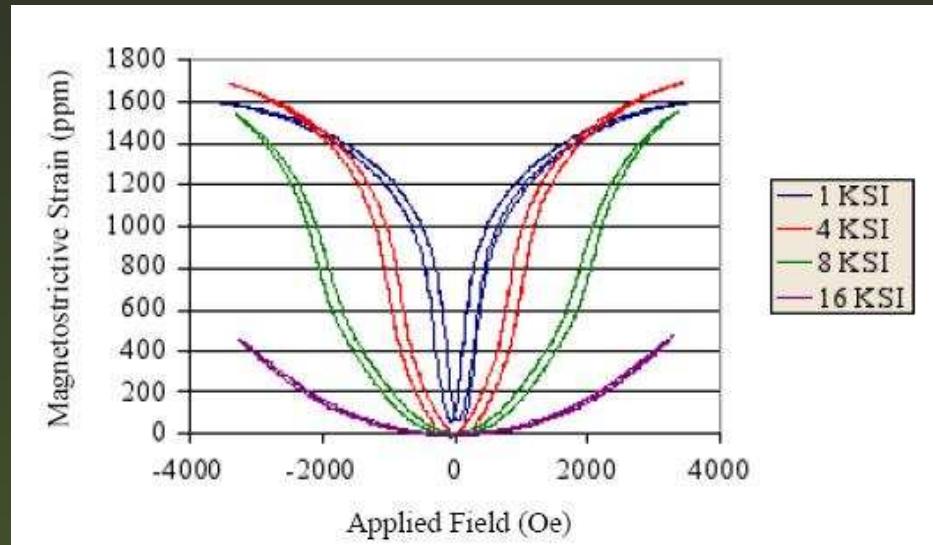
# Terfenol-D properties

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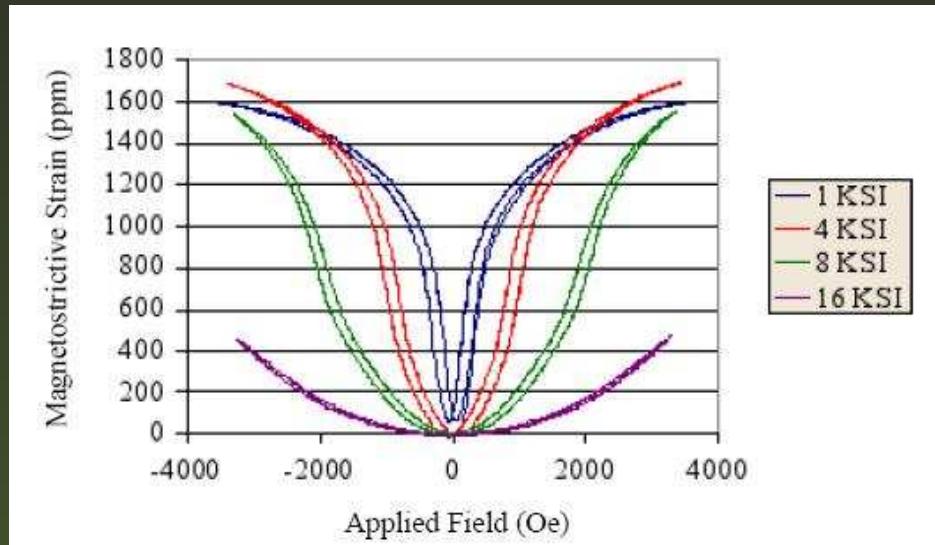
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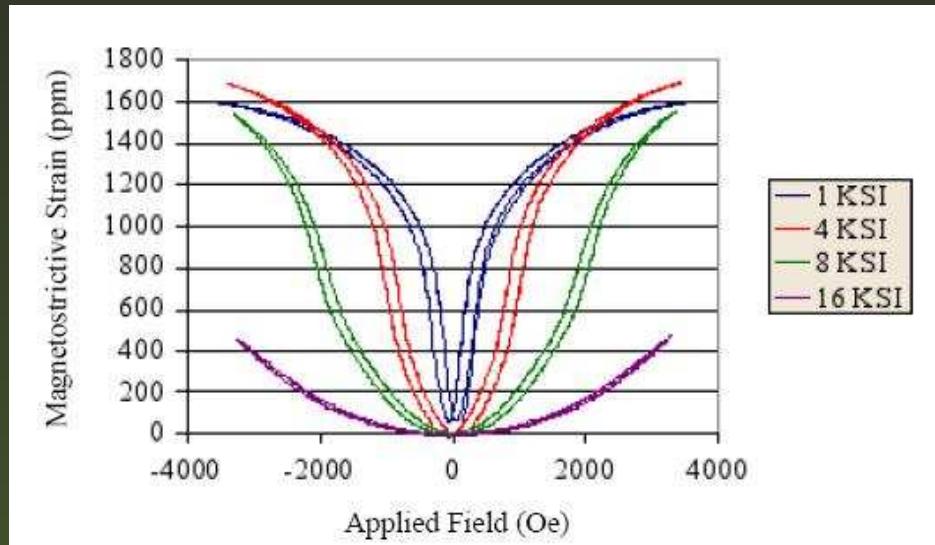
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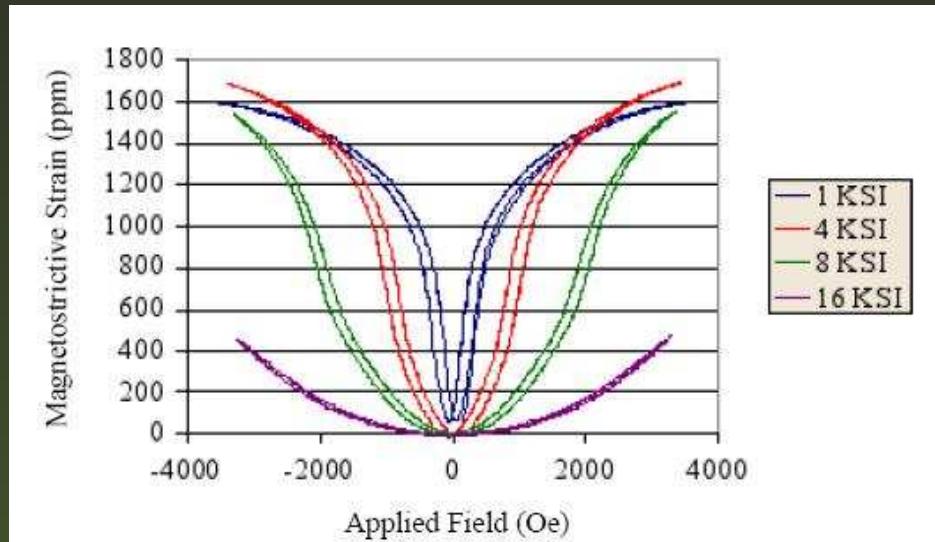
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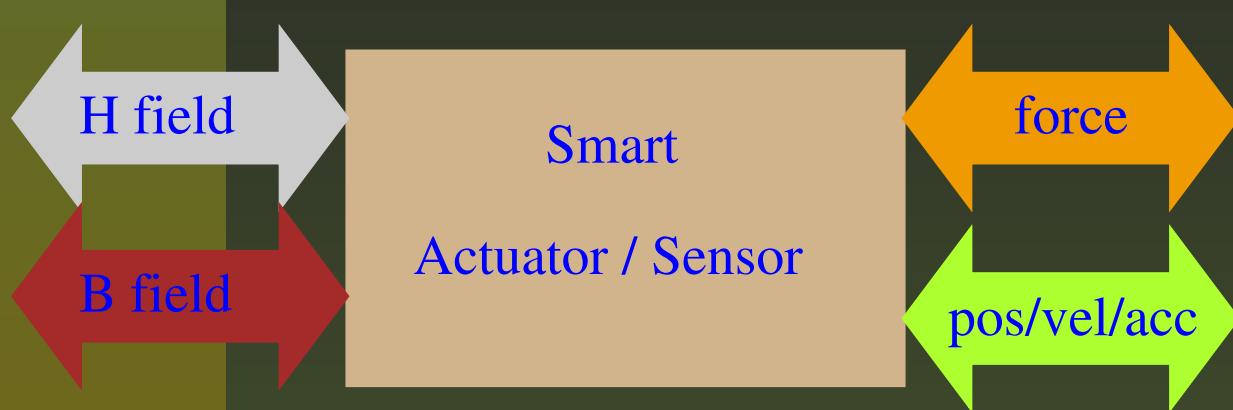
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- magneto-elastic (Joule effect), elasto-magnetic coupling (Villari effect)

# Why smart actuators / sensors ?



- Sensing and actuating capabilities can be combined in one device
- ... with a *smart* integration of magneto-elastic materials properties and feedback techniques
- embedded smart controller (microprocessors), power section on board, etc.
- one device can be used for different tasks!
  - ... software update

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- Micropositioning (SRF, tooling machines, robots, etc.)
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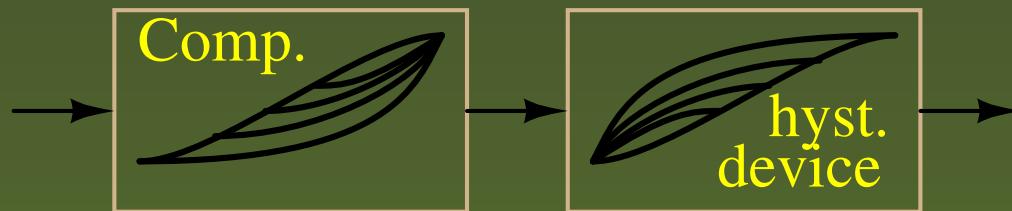
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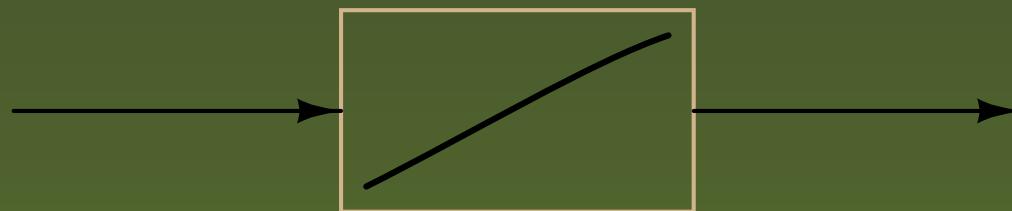


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D. Davino, C. Natale, S. Pirozzi, C. Visone, A fast compensation algorithm for real-time control of magnetostrictive actuators, J. Mag. and Mag. Mat., vol. 290-291, (2005)

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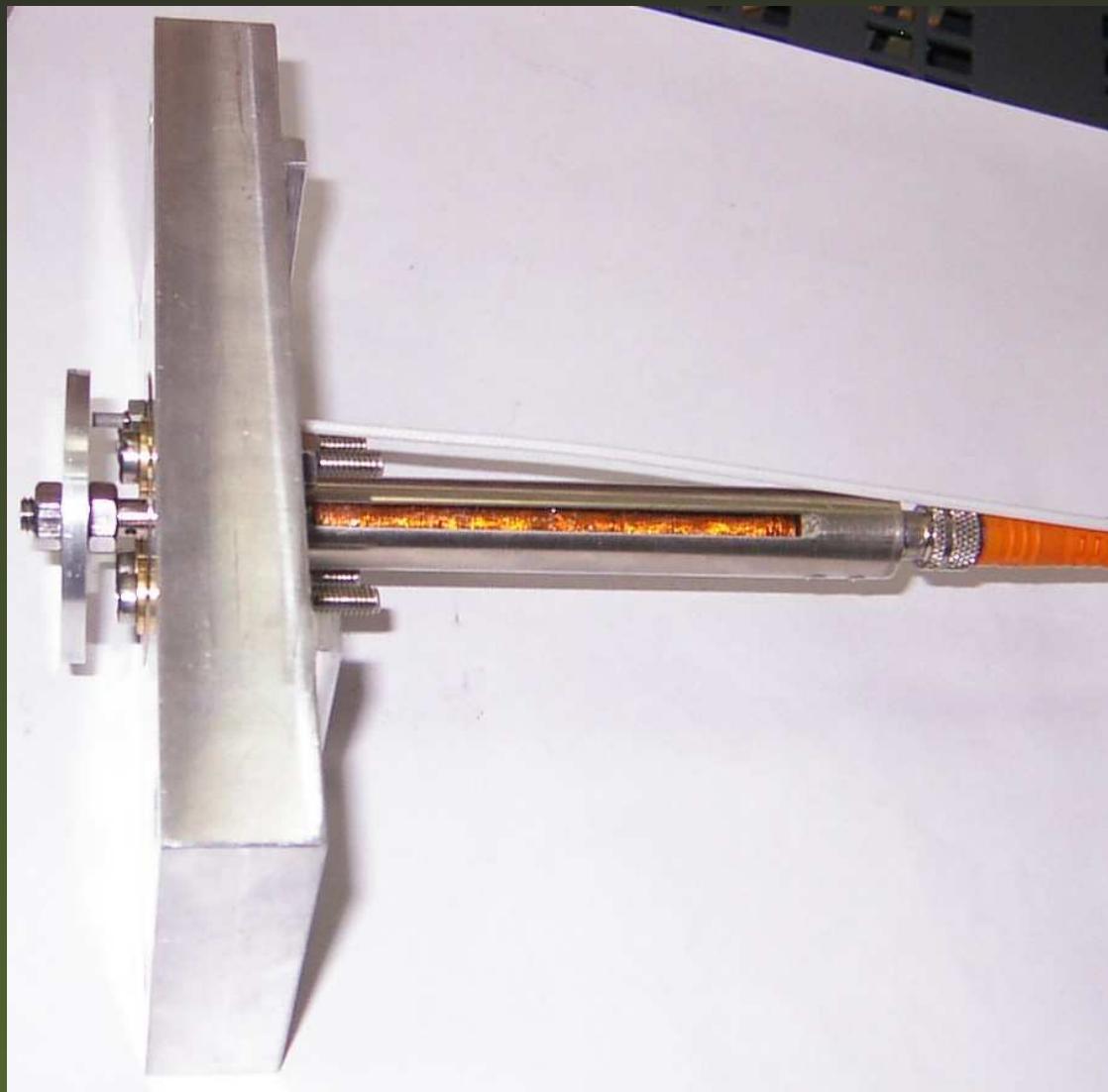
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*Other methods:* fuzzy, neural networks

- pros: adaptiveness, identification noise rejection
- cons: **implementation** and/or computational effort

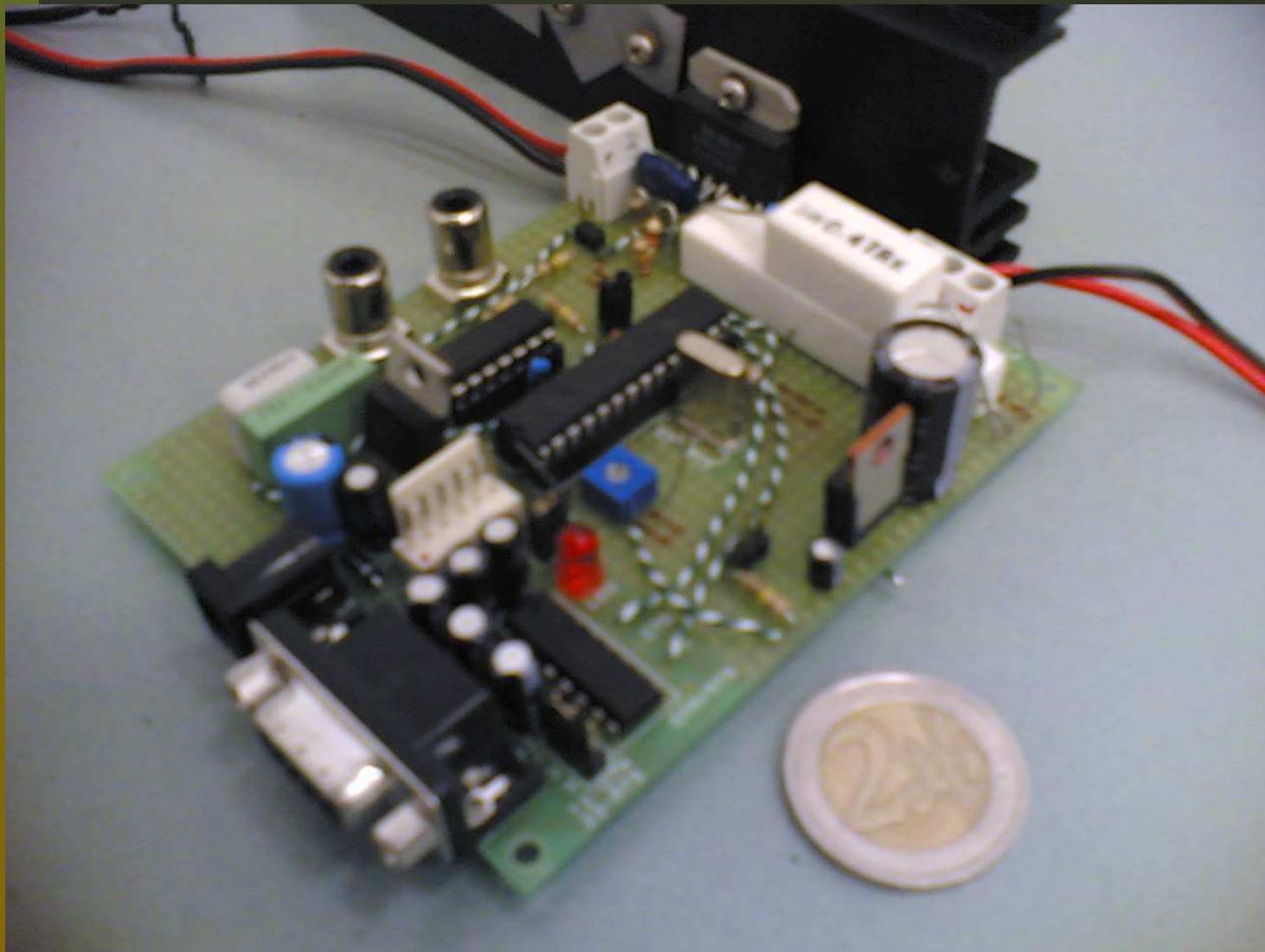
# A compensated (linear) actuator

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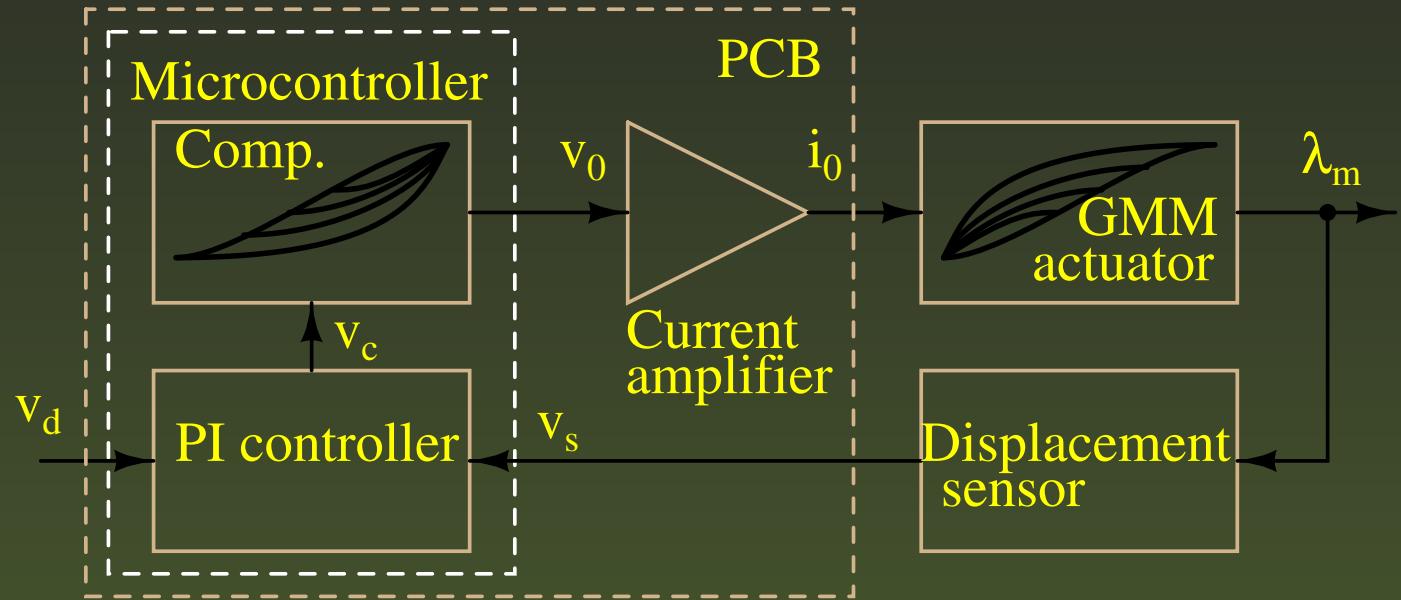


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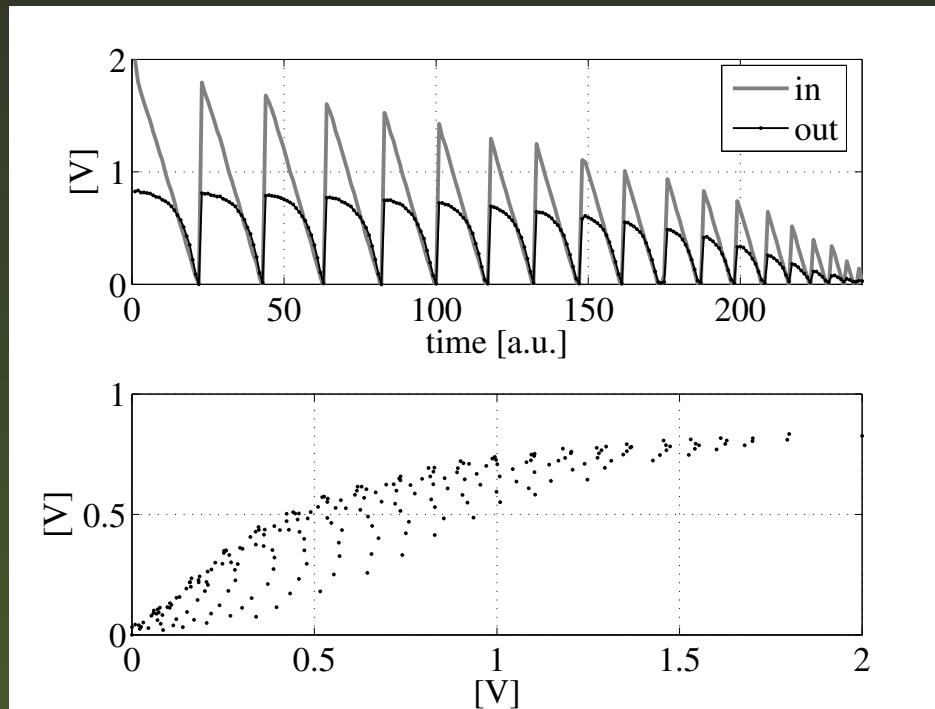
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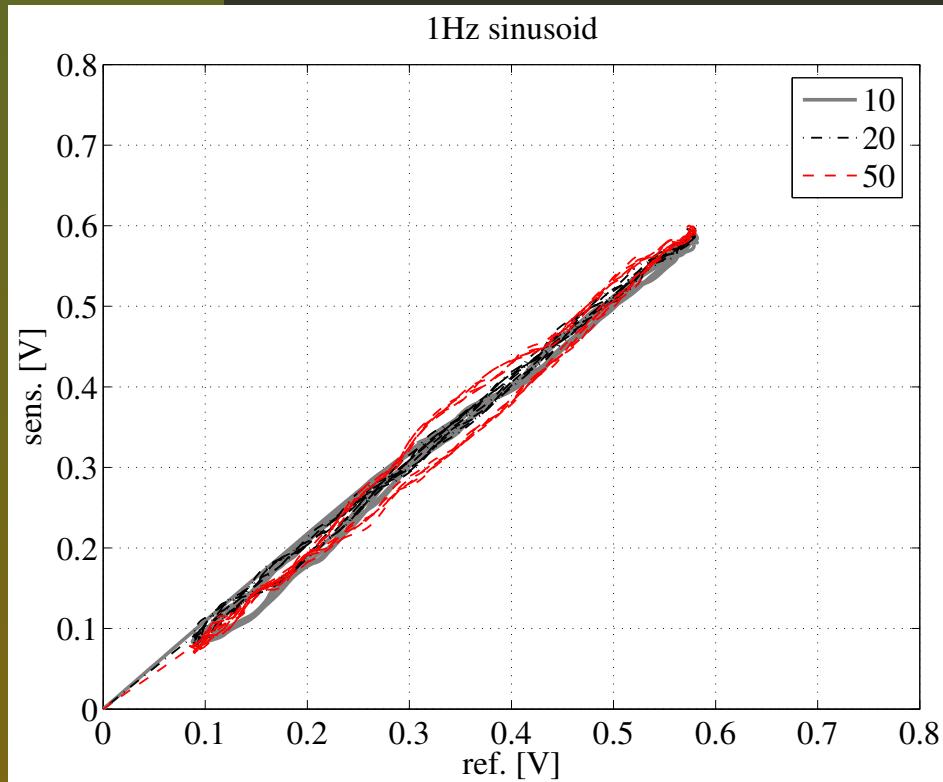
- 16 bit PIC microcontroller (30MFlops, 40MHz clock), four 10bit A/D converters (0-5V range), one PWM modulator
- eddy current proximity sensor
- 2A/V gain current amplifier on board (4A max)
- $20\mu\text{m}$  max displacement

# Identification

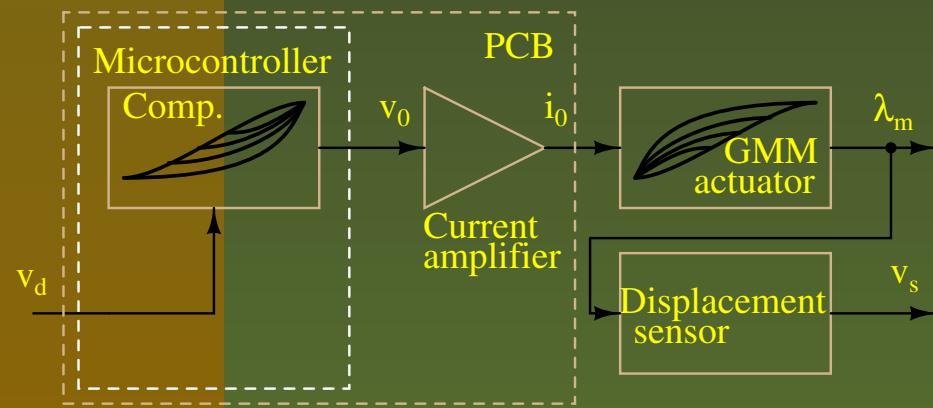
first order reversal curves:



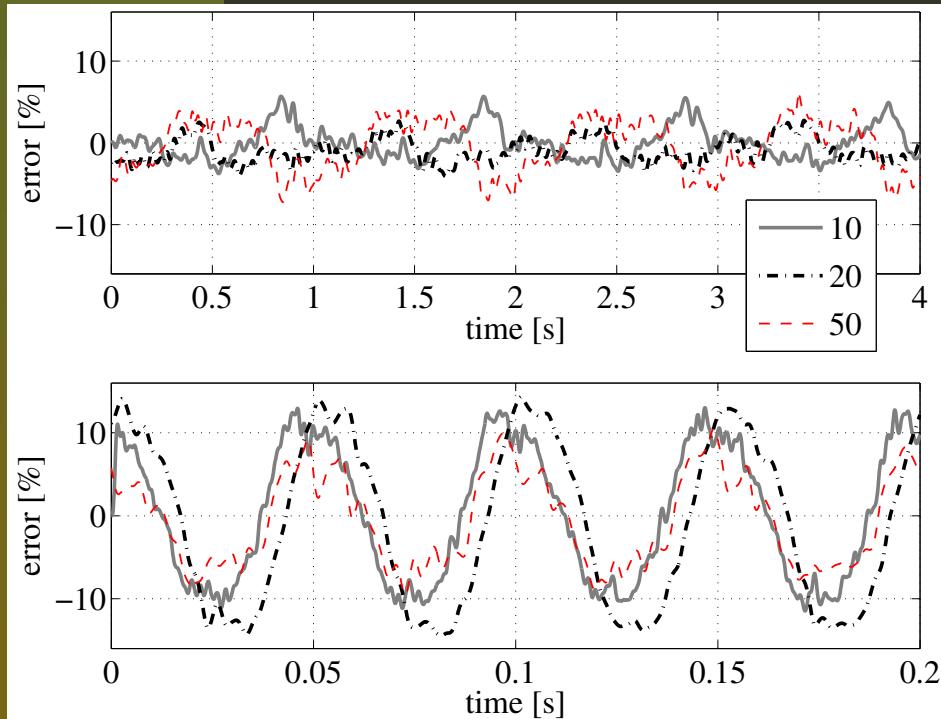
# Experimental results: sinusoid



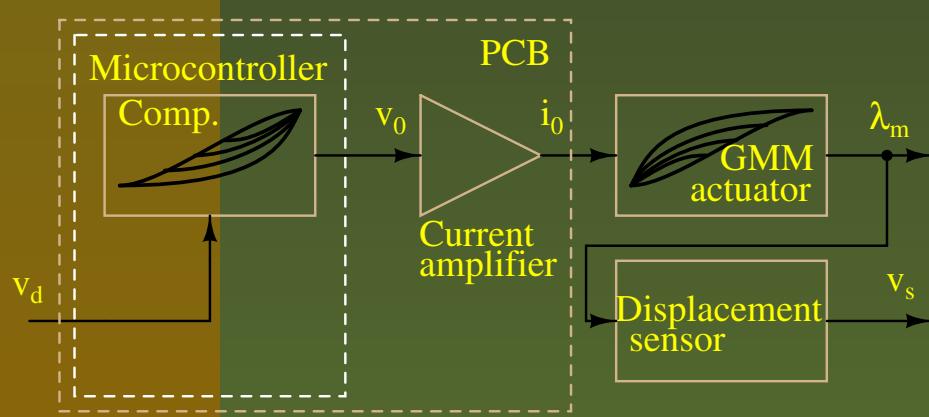
- open loop configuration
- identification matrices:  
10x10, 20x20 and 50x50
- without interpolation
- 1Hz sinusoid reference



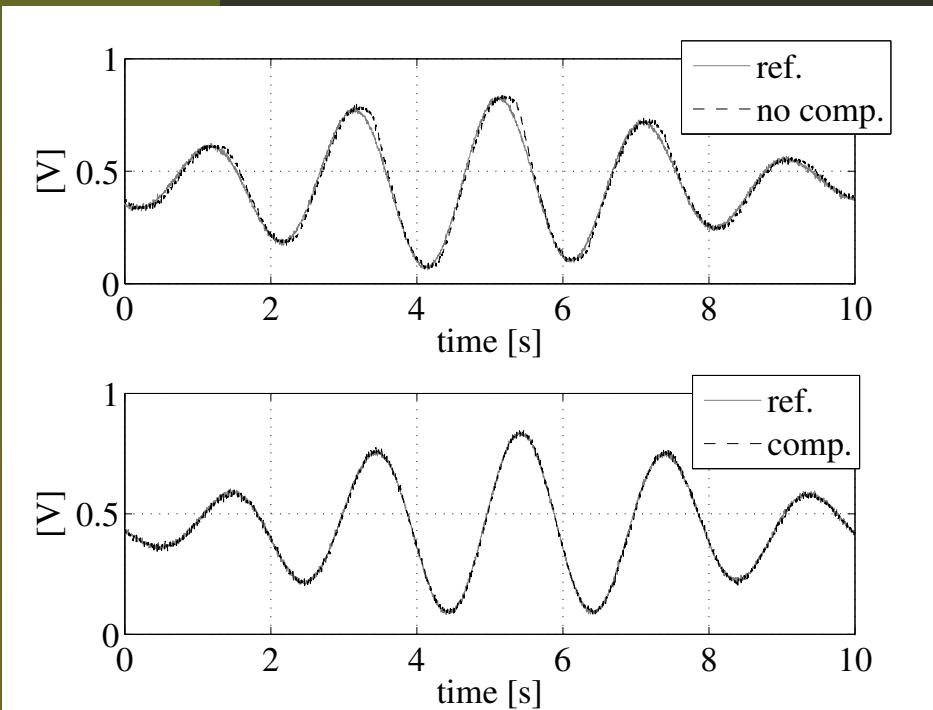
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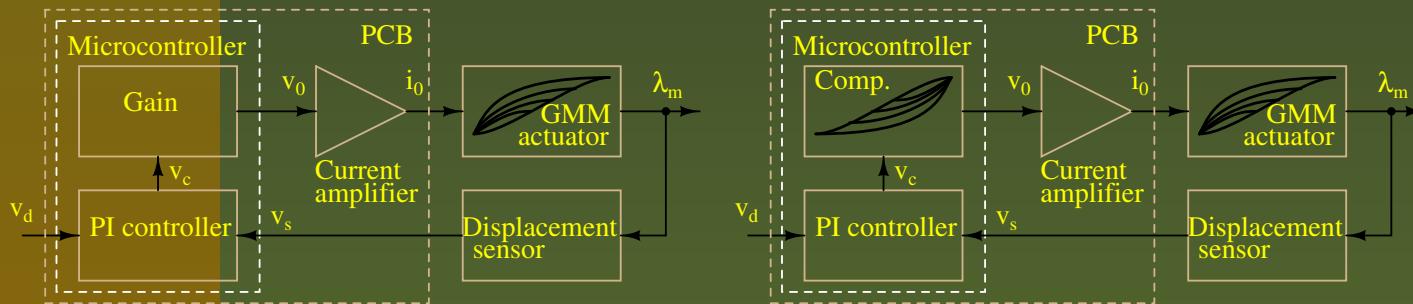
- open loop configuration
- identification matrices:  
10x10, 20x20 and 50x50
- without interpolation
- 1Hz and 20Hz reference



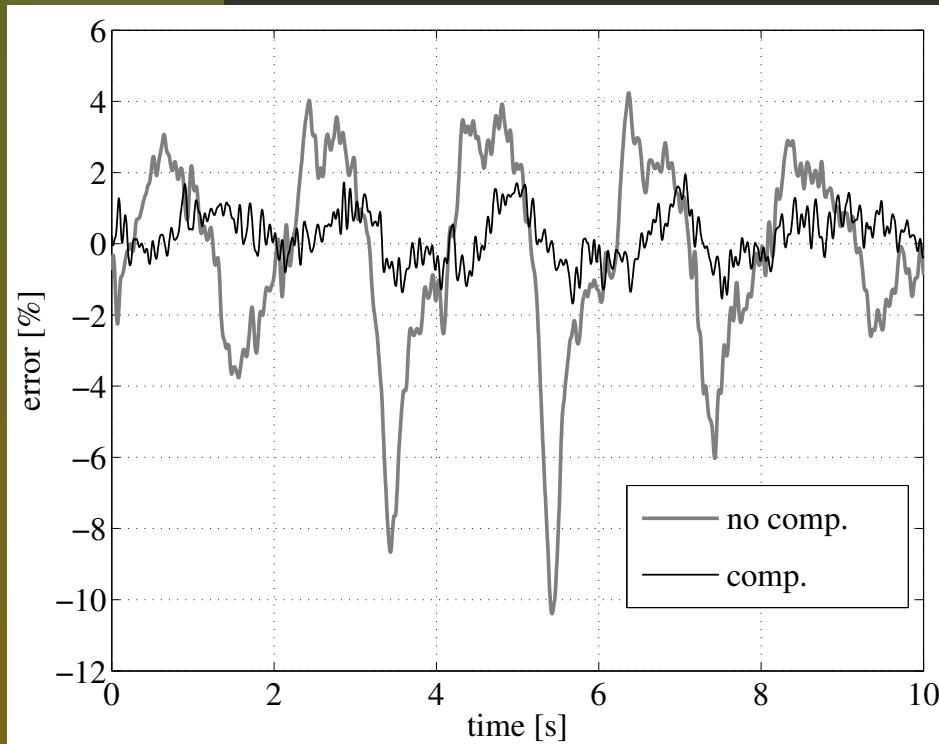
# Experimental results: AM-like signal



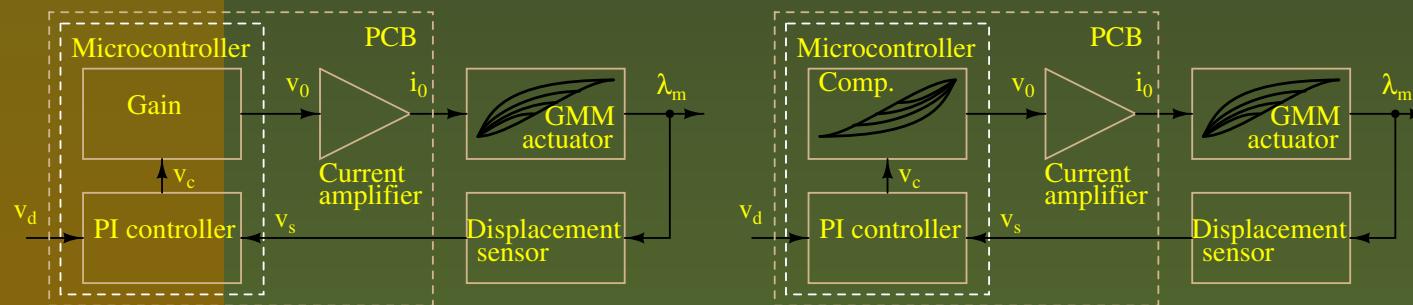
- closed loop configuration
  - comp. vs no comp.
- 10x10 identification matrix
- tracking is good



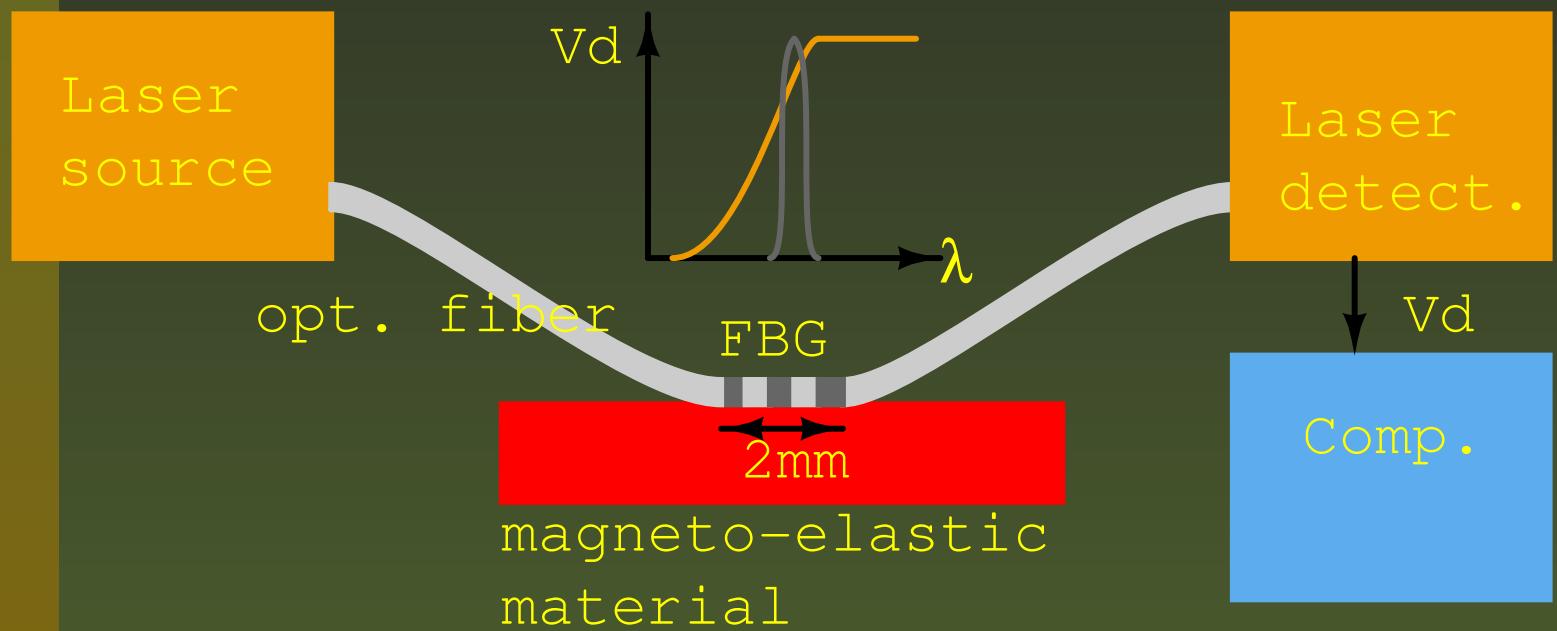
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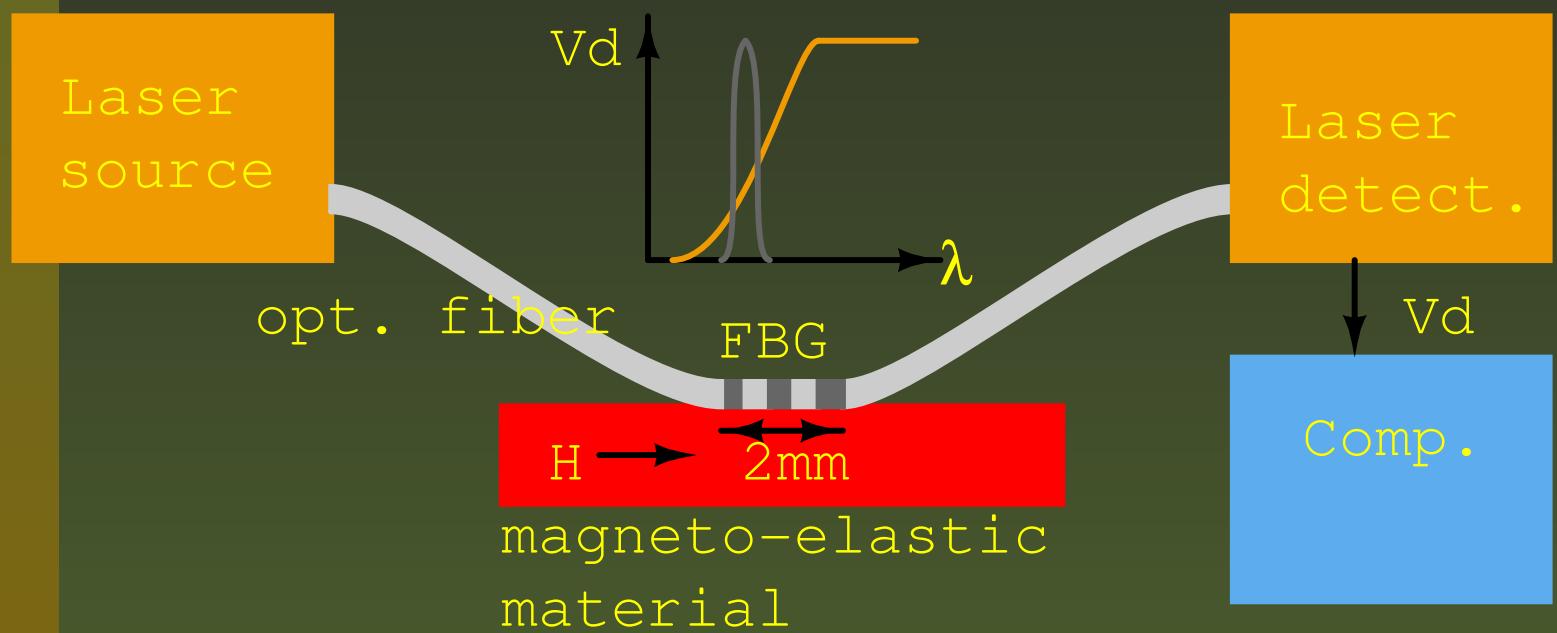
- closed loop configuration
  - comp. vs no comp.
- 10x10 identification matrix
- compensated case shows halved error



# A magnetic field sensor proof



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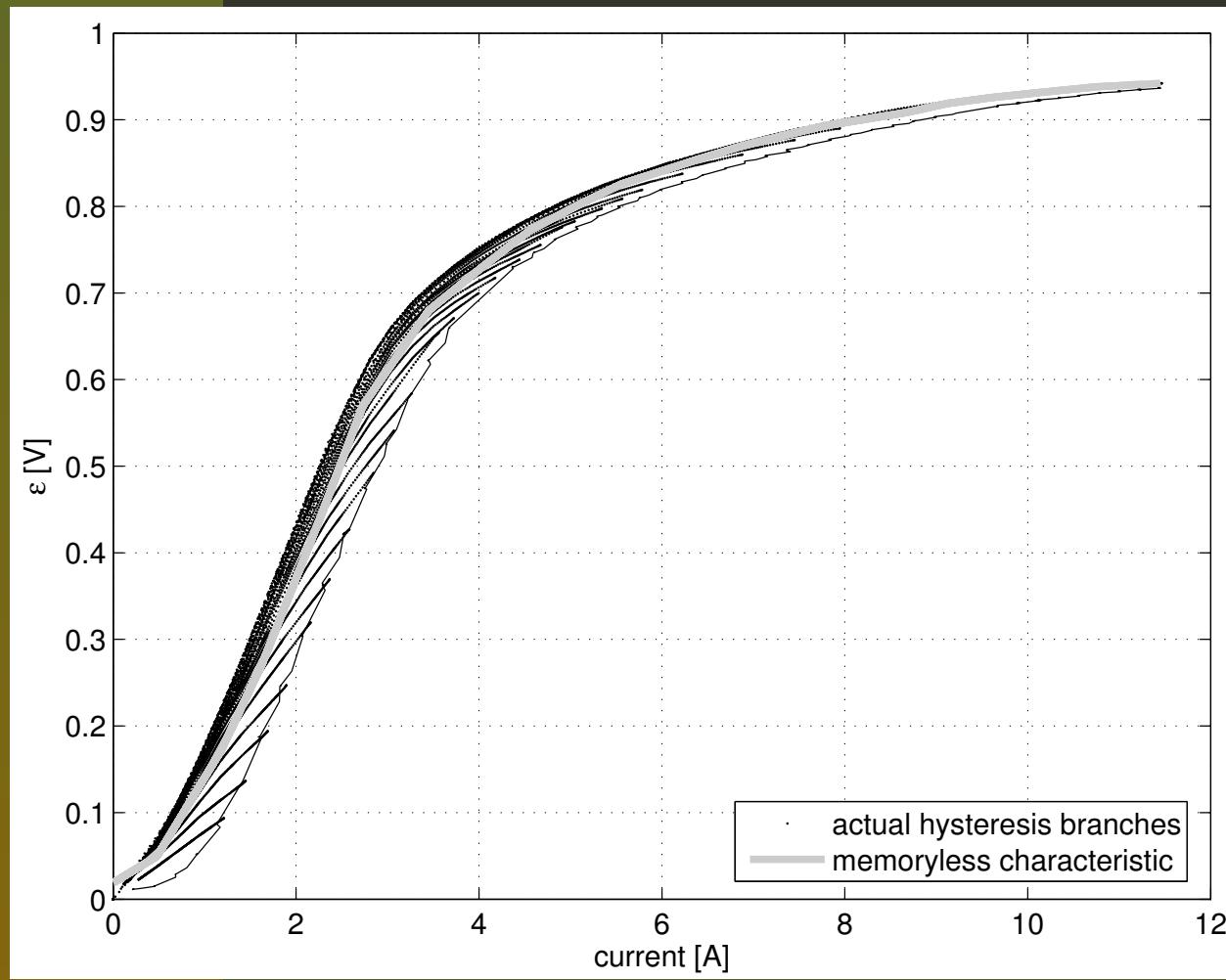


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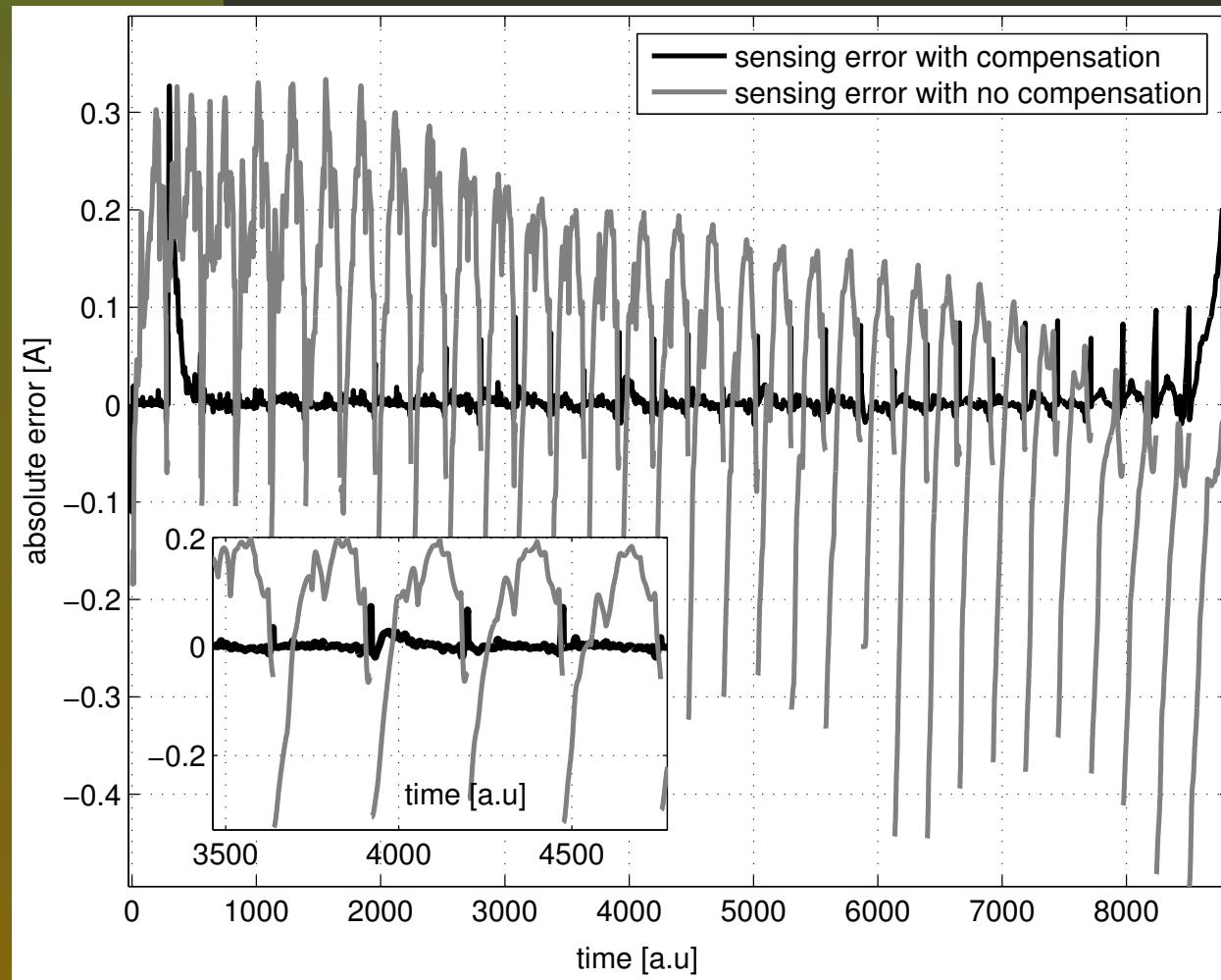
- optic Fiber Bragg Gratings (FBG) as strain sensor:  $\Delta\lambda/\lambda \propto \varepsilon$ .
- compression test machine as preload
- 360 coils air solenoid as *unknown* magnetic field source
- 4.7mm diameter and 20mm length Terfenol-D rod

# Experiment: identification input



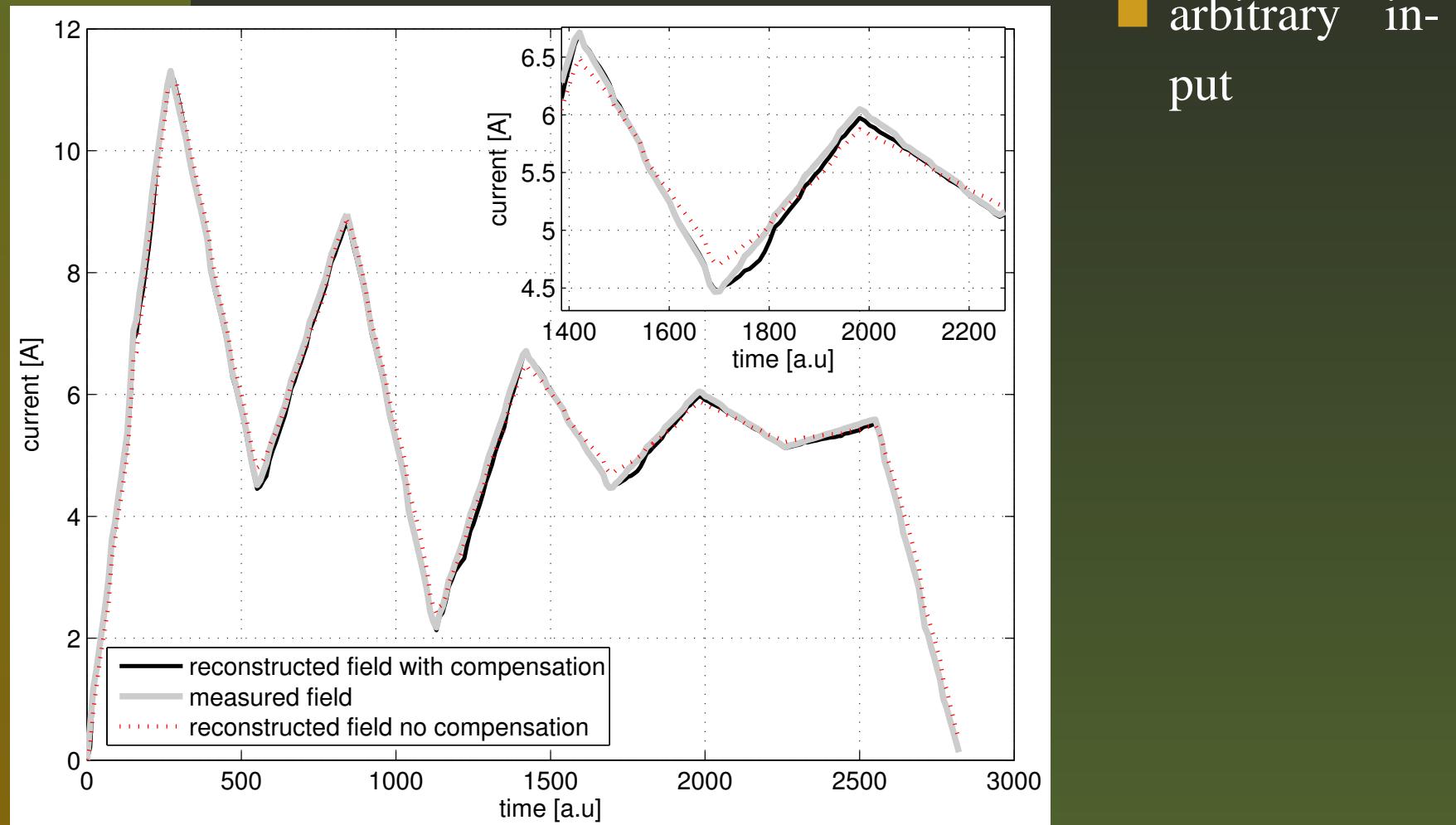
- f.o.r. curves
- memoryless characteristic as reference

# Experiment: identification input



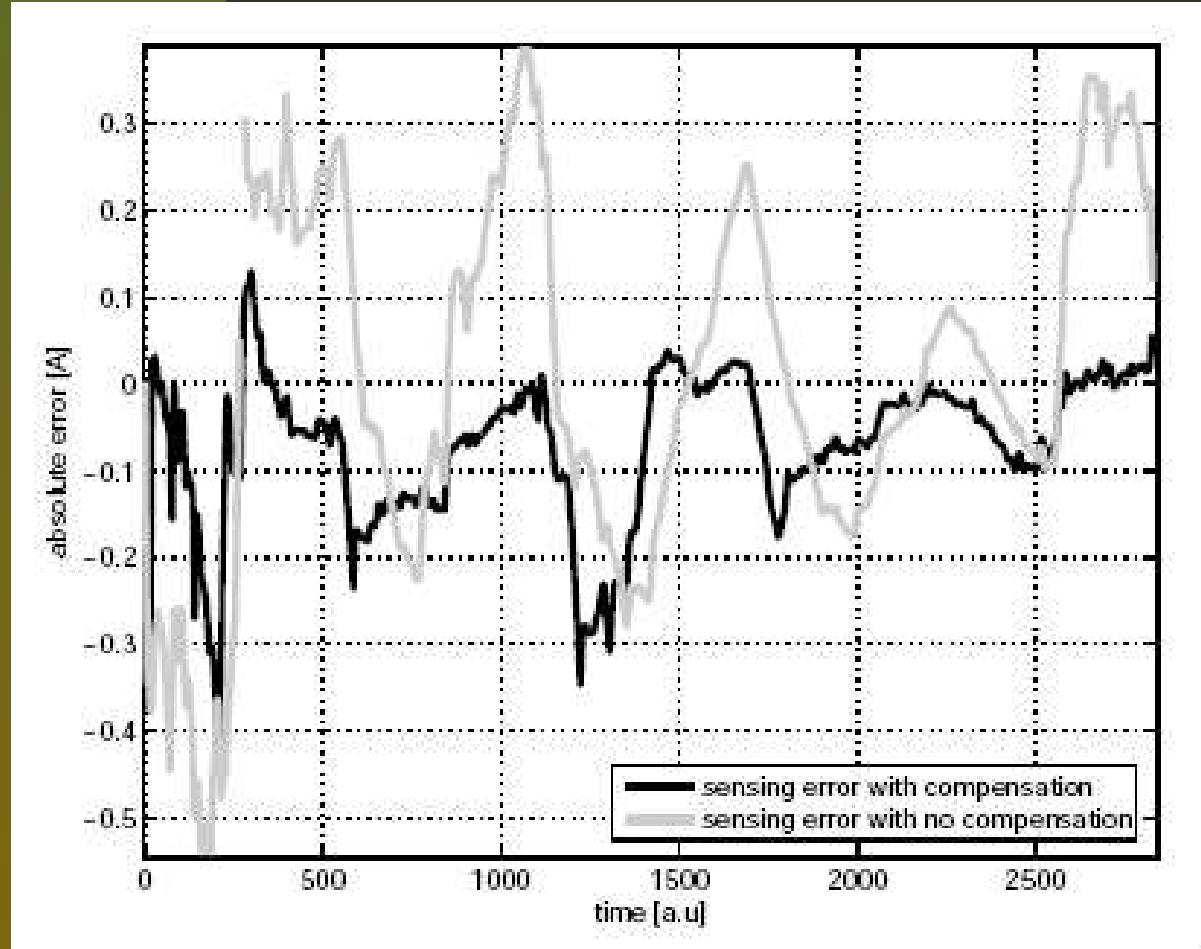
- f.o.r. curves
- the absolute error is much lower on the identification input

# Experiment: arbitrary input



■ arbitrary in-  
put

# Experiment: arbitrary input



■ compensated case shows halved error

# Collaborations



■ Optoelectronic group: C. Ambrosino, S. Campopiano, A. Cusano, A. Cutolo



Automatic group: C. Natale, S. Pirozzi.



Elettrotechnic group: C. Serpico, M. d'Aquino



V. Basso, M. Pasquale, C. Sasso



A. Adly

# Conclusions

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- Magneto-elastic materials can be used in actuators and sensors
- A phenomenological model can compensate the hysteresis  $\Rightarrow$  better performance
- A linear actuator application has been presented
- A linear magnetic field sensor application has been presented

# References Thank you!

- C. Natale, F. Velardi, C. Visone, Physica B: Condensed Matter 306 (2001) 161.
- A. Cavallo, C. Natale, C. Pirozzi, C. Visone, IEEE Transactions on Magnetics 39 (2003) 1389.
- D. Davino, C. Natale, S. Pirozzi, C. Visone, Phenomenological dynamic model of a magnetostrictive actuator, Physica B: Condensed Matter, Volume 343, Issues 1-4, 1 January 2004, pp. 112-116.
- D. Davino, C. Natale, S. Pirozzi, C. Visone, Rate-dependent losses modelling for magnetostrictive actuators, J. Mag. and Mag. Mat., Vol. 272-276, Supplement 1, May 2004, pp. E1781-E1782.
- D. Davino, C. Natale, S. Pirozzi, C. Visone, A fast compensation algorithm for real-time control of magnetostrictive actuators, J. Mag. and Mag. Mat., vol. 290-291, (2005).
- D. Davino, A. Giustiniani, V. Vacca, C. Visone, Embedded hysteresis compensation and control on a magnetostrictive actuator, IEEE Transactions on Magnetics, in press.
- Two contributed oral presentations to the INTERMAG '06 conference, San Diego, 8-12 may 2006.

# Application to SRF

www.energeninc.com



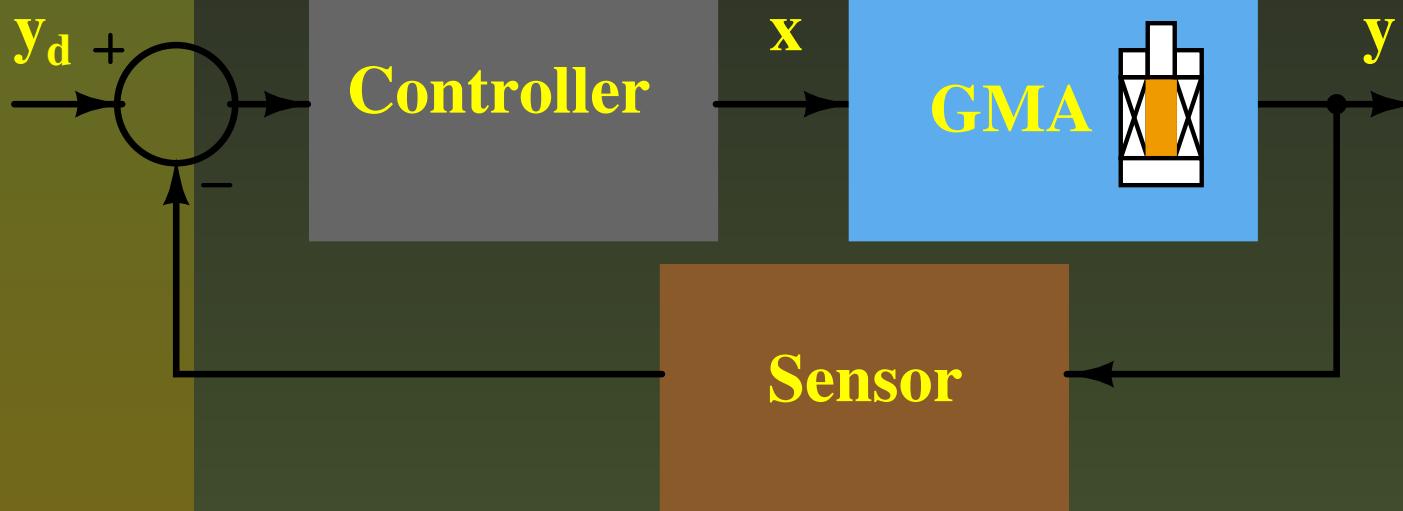
## Motor Specifications

Travel:	50 mm
Resolution:	better than 0.1 $\mu\text{m}$
Operating Temp:	2.1 K
Force:	4.4 - 13.3 kN
Speed:	0.1 mm/s

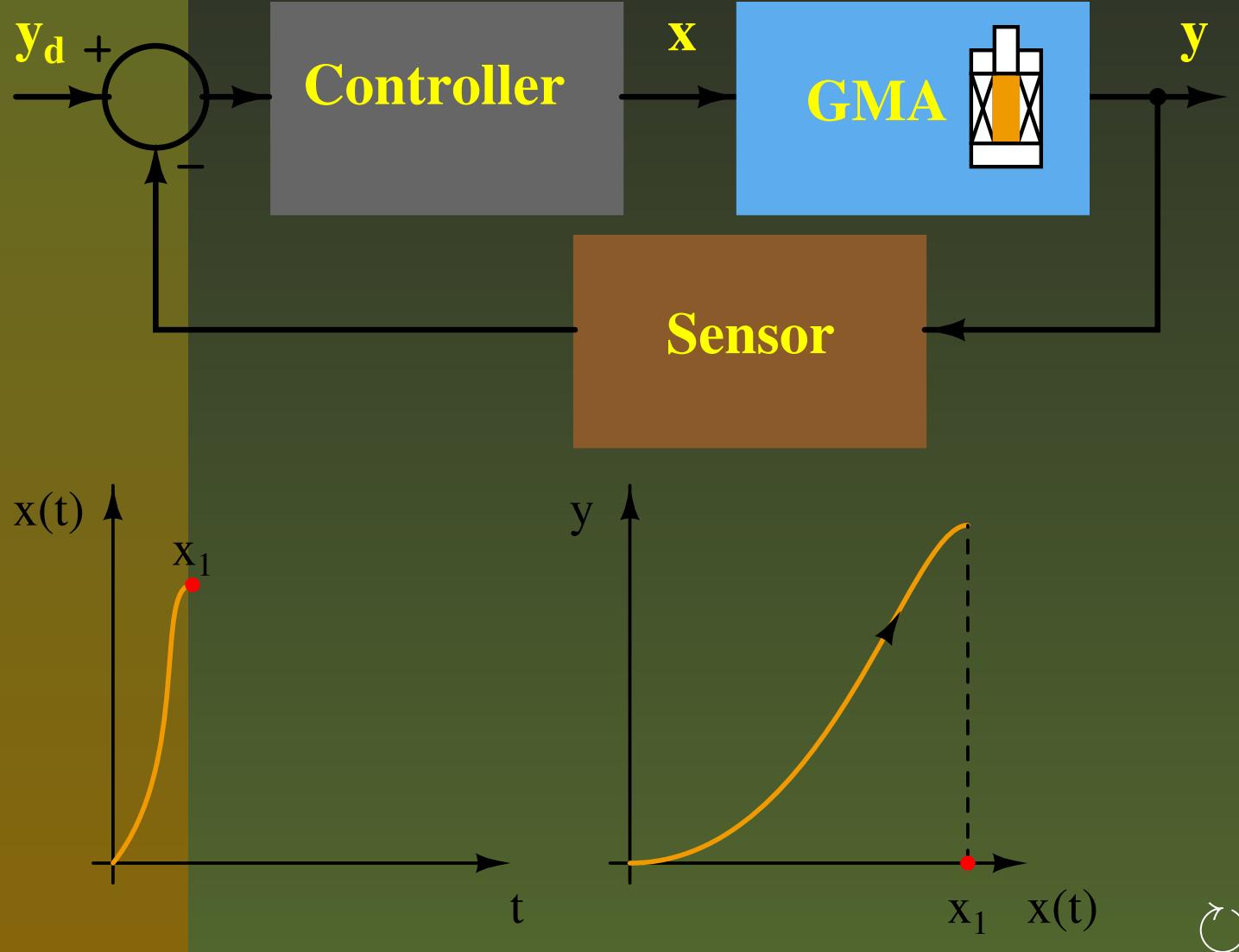
- coarse and fine tuning in a single device
- no sliding or rotating penetrations through the vacuum cryostat
- zero-power position lock-in



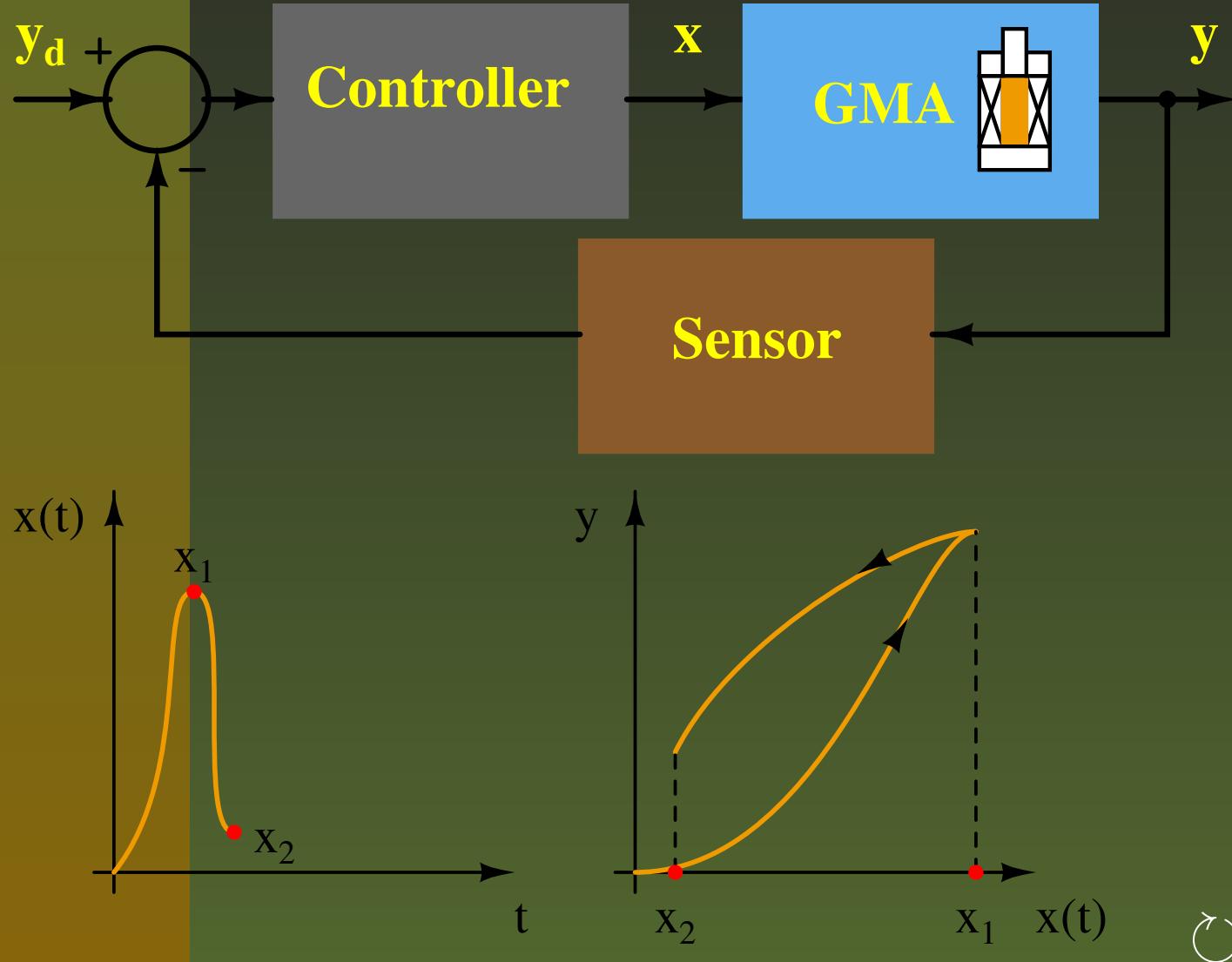
# Systems with hysteresis



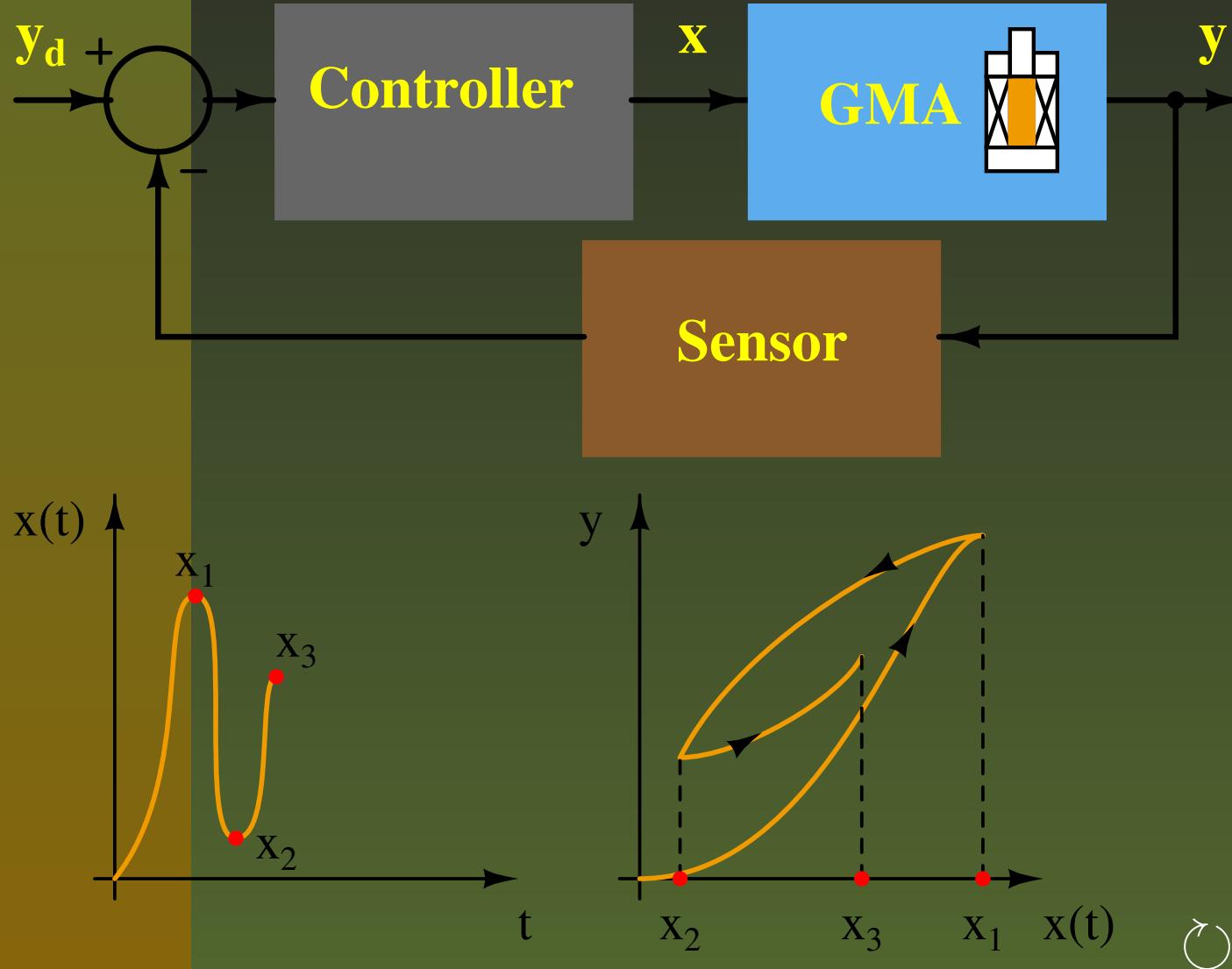
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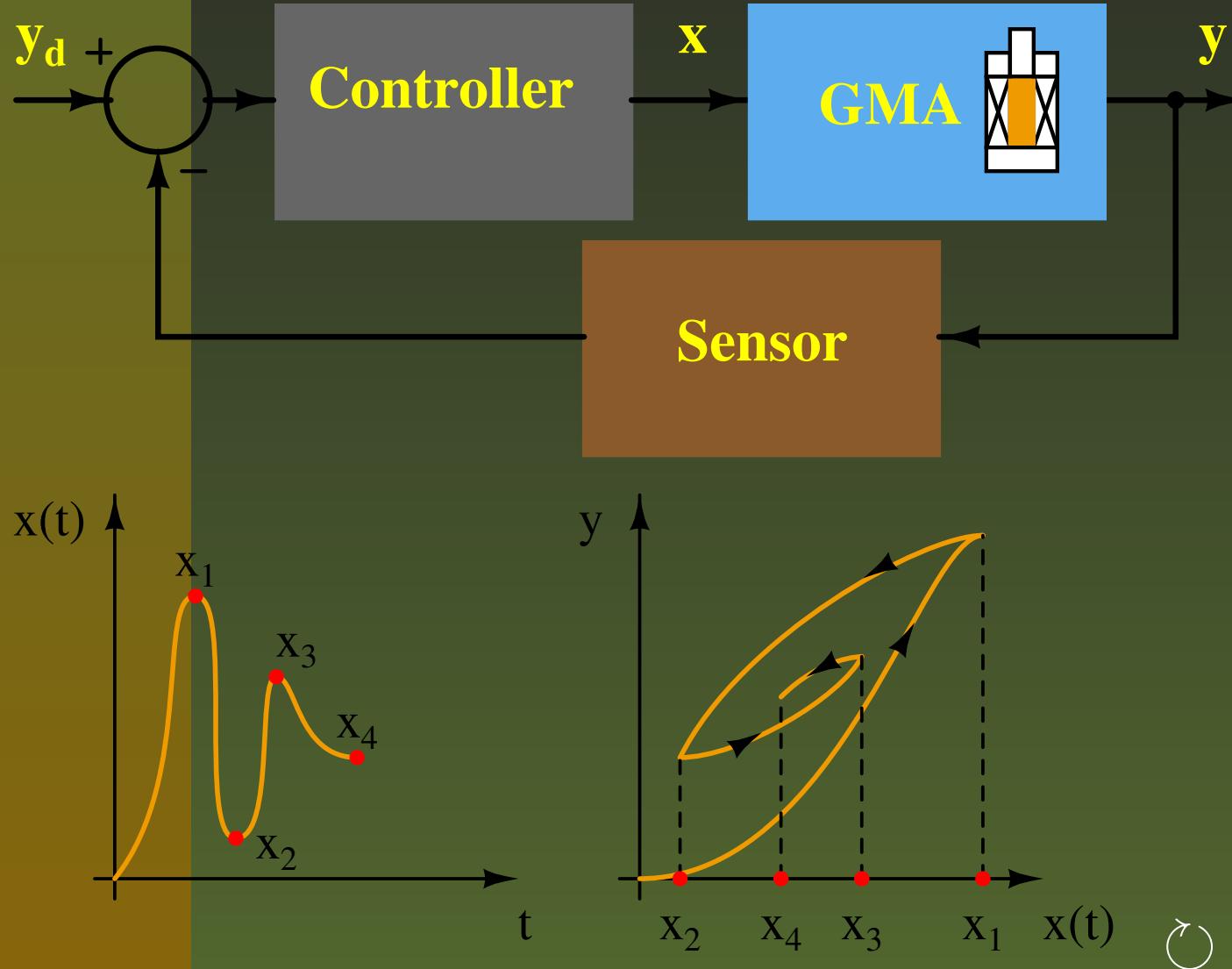
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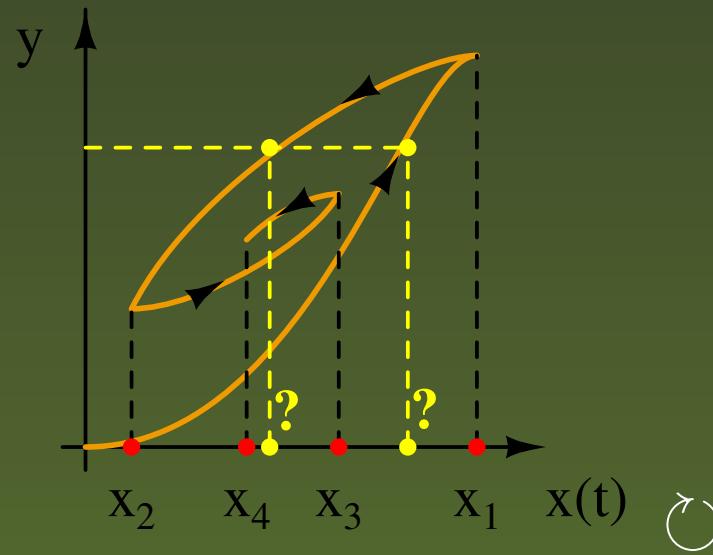
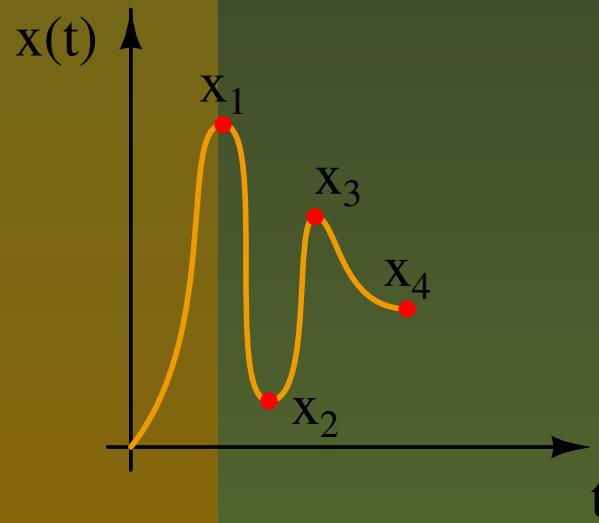
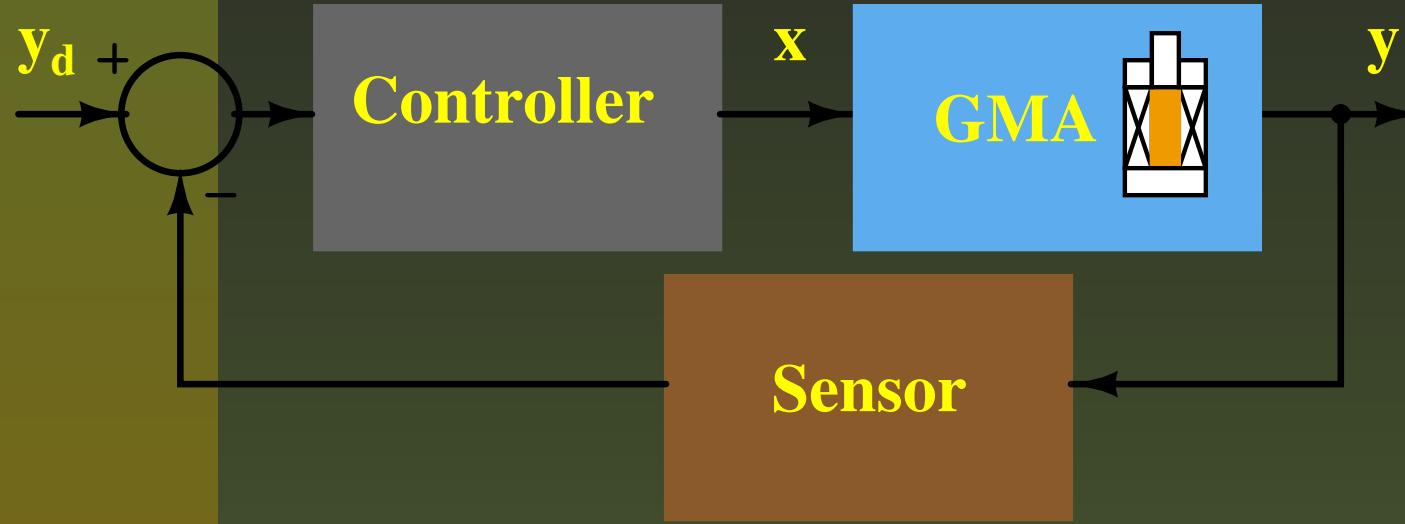
# Systems with hysteresis



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# Smart materials comparison

## AdaptaMat

Properties of smart actuator materials

	Bulk Piezo (PZT)	Multilayered piezo	Magnetostrictive Terfenol-D	MSM (Ni-Mn-Ga)
<b>Control Field</b>	Electric	Electric	Magnetic	<b>Magnetic</b>
<b>Max. strain <math>\epsilon</math> (<math>\mu\text{m}/\text{mm}</math>), linear</b>	<b>0.3</b>	<b>1.25</b>	<b>1.6</b>	<b>100</b>
<b>Work output, <math>\sigma_{bl} \times \epsilon_f</math> (<math>\text{MPa} \times \mu\text{m}/\text{mm}</math>)*</b>	6	25	112	300
<b>Young's modulus (GPa)</b>	48-74	45-62	25-35	<b>7.7**</b>
<b>Tensile strength (MPa)</b>	5-50	5-30	28	
<b>Compressive strength (MPa)</b>	60	50	700	<b>700</b>
<b>Curie Temperature (°C)</b>	200-350	200-350	380	<b>103#</b>
<b>Max. operating temperature (°C)</b>	100	100	150	<b>70#</b>
<b>Resistivity (<math>\Omega \cdot \text{m}</math>)</b>	$10^{10}$	$10^{10}$	$58 \times 10^{-8}$	<b><math>80 \times 10^{-8}</math></b>
<b>Relative permittivity</b>	800-2400	800-2400	NA	NA
<b>Relative permeability</b>	1	1	3-10	<b>1.5-40</b>
<b>Coupling factor (%)</b>	75	70	75	<b>75</b>
<b>Max. energy density (kJ/m<sup>3</sup>)</b>	2	18.5	27	<b>90</b>
<b>Field strength for max. strain</b>	2 MV/m	2 MV/m	240 kA/m	<b>400 kA/m</b>

\*  $\sigma_{bl}$ : blocking stress (in MSM defined as the stress at which strain is 0.01  $\epsilon_f$ ),  $\epsilon_f$ : maximum strain

\*\* Measured when MSM sample oriented at a single martensite variant

# can be increased by changing the proportion of Ni-Mn-Ga elements